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A NUMERICAL STUDY OF AN IDEALIZED EMP PROBLEM.(U)  
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Compared, and it is set forth that the exponential differencing method provides a more efficient solution to the ordinary differential equations of the type involved in this problem.

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## FOREWORD

The Army Multiple Systems Evaluation Program (MSEP) is a comprehensive program developing general analytic techniques for the prediction of high-electromagnetic-pulse vulnerability and hardening technology and for the application of these techniques to a list of critical systems. The analytic techniques have been verified for a large class of tactical systems. The hardening techniques have been applied to specific systems and are now resulting in product improvement programs leading to hardened equipment in the field.

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## 1. INTRODUCTION

This effort was written under the sponsorship of the Multiple Systems Evaluation Program (MSEP) which has as its main objective to harden Army tactical systems to the exoatmospheric electromagnetic-pulse (EMP) threat. Along with this major objective, the MSEP is also tasked with the aim to develop experimental and analytical evaluation techniques that are applicable to all systems' problems. This work illuminates several numerical techniques that can be used to solve ordinary differential equations that might arise in making EMP vulnerability assessments for tactical Army systems. Therefore, the objective of providing analytic methods is satisfied.

A study was undertaken to expand upon the results obtained in a paper by Wyatt<sup>1</sup> and to investigate and compare two numerical techniques in solving ordinary differential equations that occur in an EMP problem. It was conducted with the purpose of refining the previous calculations.<sup>1</sup> The numerical techniques employed are fairly standard methods, but whereas Wyatt was concerned only with approximate solutions, this work deals mainly with the specific numerical techniques used in the solution of the problem. An analysis of truncation errors was employed to deal with the accuracy of the solutions that better solidifies the results. The methods utilized were the predictor-corrector technique known as Hamming's method and an exponential differencing method that was developed by Pope.<sup>2</sup> This effort does not attempt to explain the physics of the problem or the derivation of the ordinary differential equations. This material is fully detailed by Wyatt.<sup>1</sup>

In the following sections, some general comments are made concerning Runge-Kutta solutions and predictor-corrector solutions of ordinary differential equations. The two techniques employed in the solution of the problem are described fully, along with a discussion and comparison of the results. At the end, some conclusions are made concerning the results and the numerical methods that were used.

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<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

<sup>2</sup>David A. Pope, *An Exponential Method of Numerical Integration of Ordinary Differential Equations*, *Communications of the ACM* 6, No. 8 (August 1963), 491-493.

## 2. GENERAL PHYSICAL PROBLEM

The problem that was dealt with was the determination of the time history of the electric-field strength between two parallel, infinite, aluminum plates caused by Compton electrons generated by a transient, high-intensity, gamma-ray flux. The ordinary differential equations that are solved are a result of the application of Poisson's equation to the free charge that is the spatially distributed current of Compton electrons. Since the conductivity of the air is significant, Poisson's equation is modified by Ohm's law, which relates the air conductivity, electric-field strength, and conduction current. In the case examined here, methane was used instead of air, and it was found by Wyatt<sup>1</sup> that methane reduced the peak electric-field strength. The resulting ordinary differential equations to be solved are

$$\frac{dE(t)}{dt} + \frac{q\mu}{\epsilon} N_e(0) e^{rt} E(t) = \frac{J_c(t)}{\epsilon} e^{rt}, \quad t < 0 \quad (1)$$

$$\frac{dE(t)}{dt} + \frac{q\mu}{\epsilon} N_e(t) E(t) = \frac{J_c(t)}{\epsilon}, \quad t \geq 0, \quad (2)$$

where

$E(t)$  is the electric-field strength,

$q$  is the electronic charge,

$\mu$  is the electron mobility,

$\epsilon$  is the permittivity of free space,

$N_e(t)$  is the free electron density,

$r$  is the model parameter for gamma-flux rate history,

$J_c$  is the Compton electron current density.

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<sup>1</sup>W. T. Wyatt, Internal EMP Strength and Time Dependence for an Idealized Problem, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).



### 3. RUNGE-KUTTA AND PREDICTOR-CORRECTOR METHODS

When attempting to solve ordinary differential equations numerically, two well-known methods, the Runge-Kutta technique and the predictor-corrector technique, are often employed to find the solution. Depending on various constraints such as time, computing funds available, accuracy, and stability, there are accompanying advantages and disadvantages to both methods. Thus, before examining Hamming's method in the solution of equations (1) and (2), a few general remarks concerning fourth-order Runge-Kutta solutions and fourth-order predictor-corrector methods are made to give some background and rationale for the technique utilized.

It is generally recognized that predictor-corrector methods are more difficult to code than Runge-Kutta methods. However, although Runge-Kutta techniques are more straightforward, predictor-corrector methods provide a much easier analysis and examination of errors and are generally much faster. For example, the evaluation of  $f(x,y)$  (i.e.,  $dy/dx = f(x,y)$ ) is usually the most time-consuming part of solving differential equations, and fourth-order Runge-Kutta methods require four evaluations of  $f(x,y)$  per step, while fourth-order predictor-corrector methods require only two evaluations of  $f(x,y)$  per step. This means that the fourth-order predictor-corrector methods are generally nearly twice as fast as fourth-order Runge-Kutta techniques. Thus, the evaluation of errors and the speed of computation are two compelling reasons to use predictor-corrector methods instead of Runge-Kutta methods. However, since predictor-corrector methods are not self-starting and Runge-Kutta techniques do have the self-starting capability, Runge-Kutta methods are quite useful in generating starting values for the solution and may be used to change the interval between steps when desired. This usefulness makes Runge-Kutta methods an indispensable tool in using predictor-corrector techniques. Therefore, a combination of these two methods, (1) the Runge-Kutta to determine starting values and change the per-step interval and (2) the predictor-corrector to actually solve the differential equation and analyze the errors involved, gives a technique that is highly desirable in computing the solution of ordinary differential equations.

### 4. HAMMING'S METHOD

Since Hamming's method is not self-starting, the Runge-Kutta technique was used to start the solution. This involves writing the differential equation as

$$\frac{dy}{dx} = f(x,y)$$

and then finding

$$k_1 = f(x_1, y_1)h ,$$

$$k_2 = f(x_1 + \frac{1}{2}h, y_1 + \frac{1}{2}k_1)h ,$$

$$k_3 = f(x_1 + \frac{1}{2}h, y_1 + \frac{1}{2}k_2)h ,$$

$$k_4 = f(x_1 + h, y_1 + k_3)h ,$$

where  $h$  is the desired increment step size. Once these values are computed for a particular increment,  $\Delta y$  is calculated by

$$\Delta y = \frac{1}{6}(k_1 + 2k_2 + 2k_3 + k_4) ,$$

and then

$$y_{i+1} = y_i + \Delta y .$$

This process is continued until the desired number of starting values is obtained. In Hamming's method, three values from the Runge-Kutta technique are used to start the solution process.

Once the starting values have been determined from the Runge-Kutta technique, the general procedure for Hamming's method is used, as is done by most predictor-corrector techniques. This procedure is illustrated by the flow chart in figure 1. The specific formulas used in Hamming's method and shown in figure 1 are as follows:

$$\text{Predictor: } y_{i+1}^{(0)} = y_{i-3} + \frac{4h}{3}(2y'_i - y'_{i-1} + 2y'_{i-2}) ,$$

$$\text{Corrector: } y_{i+1}^{(j+1)} = \frac{1}{8}(9y_i - y_{i-2}) + \frac{3h}{8}([y_{i+1}^{(j)}]') + 2y'_i - y'_{i-1} ,$$

$$\text{Truncation error: } T_1 \approx \frac{9}{121}[y_{i+1} - y_{i+1}^{(0)}] ,$$

where  $h$  is the interval step size.



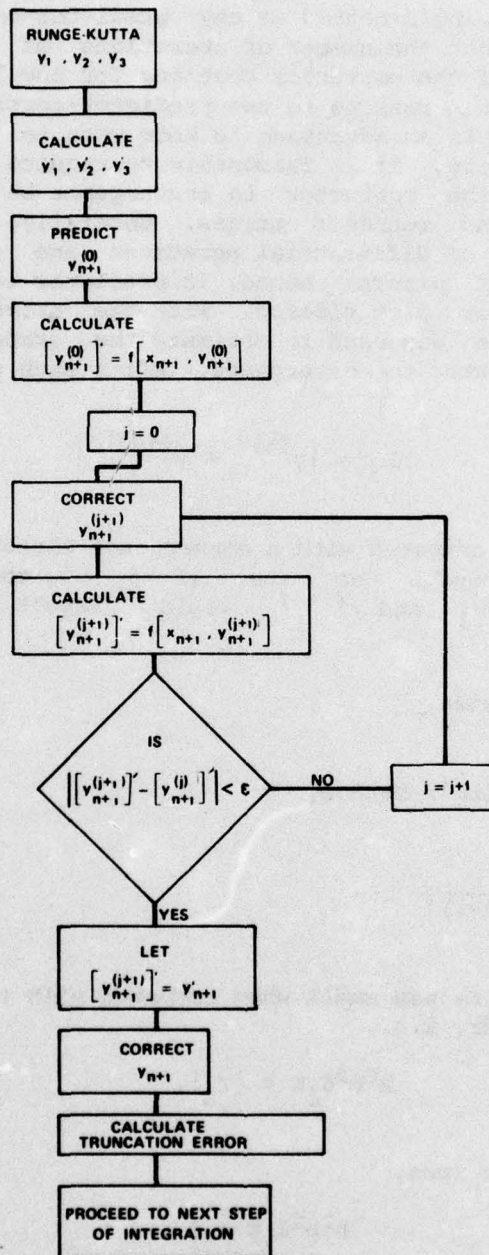


Figure 1. General Predictor-Corrector Method.

In applying Hamming's method or any predictor-corrector method, one must be cautious about the number of iterations of the corrector. To let the iteration of the corrector continue for any length of time would defeat one of the main reasons to use predictor-corrector methods, speed of computation. It is an advantage to know when to stop iterating the corrector. Therefore, it is reasonable to require that any error made by not iterating the corrector to convergence be small when compared with truncation and roundoff errors. Generally, truncation errors affect the solution of differential equations and cause instabilities more than roundoff errors; hence, in predictor-corrector techniques, only truncation error is considered. With the above point in mind, the following procedure was used to estimate the error incurred by not iterating the corrector to convergence. After each corrector iteration,

$$\delta_i = |y^{(i)} - y^{(i-1)}|$$

was computed and compared with a convergence factor,  $\epsilon$  ( $\epsilon$  in fig. 1). The value  $\epsilon$  was chosen so that if  $\delta_i < \epsilon$ , then terminating the iteration with  $[y^{(i)}]'$  and  $y^{(i+1)}$  would result in an error value of  $h^2 b^2 \delta_i K$ , where

$h$  = time step size,

$b = \frac{3}{8}$  for Hamming's method,

$$K = \frac{\delta_i}{|y^{(i)} - y^{(i-1)}|}.$$

This value,  $h^2 b^2 \delta_i K$ , was small when compared with the absolute value of the truncation error, i.e.,

$$h^2 b^2 \delta_i K < |T_n|.$$

In all the computer runs,

$$h^2 b^2 \delta_i K = 0,$$

which was indeed less than the absolute value of the truncation error in every instance of the calculations. Also, utilizing this procedure, only two iterations of the corrector were required for convergence in most cases.



## 5. EXPONENTIAL DIFFERENCING METHOD

The second method used to solve differential equations (1) and (2) was an exponential differencing technique developed by Pope.<sup>2</sup> This method has been shown to have superior stability properties for large step sizes when dealing with a large class of differential equations. Hence, this technique may be used with a large step size to decrease significantly the total computing time for a solution, particularly in those engineering problems, like EMP problems, where high accuracy is not necessarily needed. However, in this work, the accuracy is a significant part of the effort, and, as it turns out, the exponential differencing method does provide precise results, which are shown in section 7. The exponential differencing technique is now described.

Consider

$$y' = f(x, y) \quad (3)$$

with the initial condition  $y(x_0) = y_0$ . The exponential difference equation used to solve equation (3) is given by

$$y_{n+1} = y_n + hf + y'' f_y^{-2} \left( e^{hf} y - 1 - hf_y \right), \quad (4)$$

where

$h$  is the time step size,

$$y'' = f_x + f \cdot f_y,$$

$f_x, f_y$  are the partial derivatives of  $f$  with respect to  $x$  and  $y$ . The truncation error for this algorithm is

$$T_{n+1} \approx \frac{1}{6} h^3 \left( f_{xx} + 2f \cdot f_{xy} + f^2 \cdot f_{yy} \right).$$

If the value of  $|hf_y|$  is small, at least if  $|hf_y| < 0.1$ , then in place of the exponential formula, the series form

$$y_{n+1} = y_n + hf + y'' \sum_{k=2}^{\infty} \frac{h^k f_y^{k-2}}{k!} \quad (5)$$

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<sup>2</sup>David A. Pope, An Exponential Method of Numerical Integration of Ordinary Differential Equations, Communications of the ACM, 6, No. 8 (August 1963), 491-493.

is used to avoid loss of significance due to cancellation of terms. In this case, only a few terms of the series are needed; we used only three. If the value of  $hf_y$  is fairly large, then the exponential subroutines should be used.

To find the solutions for equations (1) and (2) using the exponential differencing method, we let

$$f(t, E) = \frac{dE}{dt} = \frac{J}{\epsilon} e^{rt} - \frac{q\mu}{\epsilon} N_e(0) e^{rt} E, \quad t < 0,$$

$$g(t, E) = \frac{dE}{dt} = \frac{J}{\epsilon} - \frac{q\mu}{\epsilon} N_e(t) E, \quad t > 0.$$

The various equations needed to use equations (4) and (5) are now generated. For the function  $f(t, E)$ , its derivatives and partial derivatives are

$$f_t = \frac{r}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E],$$

$$f_E = -\frac{q\mu}{\epsilon} N_e(0) e^{rt},$$

$$E'' = f_t + f \cdot f_E = \frac{r}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E] + \frac{q\mu}{\epsilon^2} N_e(0) e^{2rt} [q\mu N_e(0) E - J_c],$$

$$f_{tt} = \frac{r^2}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E],$$

$$f_{EE} = 0,$$

$$f_{tE} = -\frac{q\mu}{\epsilon} N_e(0) r e^{rt}.$$

The truncation error is

$$T_{n+1} \approx \frac{1}{6} h^3 \frac{r^2}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E] + \left\{ \frac{2q\mu}{\epsilon^2} N_e(0) e^{2rt} [q\mu N_e(0) E - J_c] \right\}.$$



For the function  $g(t, E)$ , its derivatives and partial derivatives are found to be

$$g_t = -\frac{qu}{\epsilon} EN'_0(t) = -\frac{qu}{\epsilon} S \cdot E ,$$

$$g_E = -\frac{qu}{\epsilon} N_0(t) ,$$

$$E'' = g_t + g \cdot g_E$$

$$= -\frac{qu}{\epsilon} S \cdot E + \frac{qu}{\epsilon} N_0(t) [quN_0(t)E - J_c] ,$$

$$g_{tt} = 0 ,$$

$$g_{EE} = 0 ,$$

$$g_{tE} = -\frac{qu}{\epsilon} S ,$$

where  $N_0(t)$  is described in section 6. The truncation error is given by

$$T_{n+1} \approx \frac{1}{6} h^3 \left\{ \frac{2qu}{\epsilon^2} [quN_0(t)E - J_c] \right\} .$$

It is an easy, straightforward process to code these quantities to calculate equations (4) and (5). The general procedure used to solve the exponential difference equation is given in figure 2.

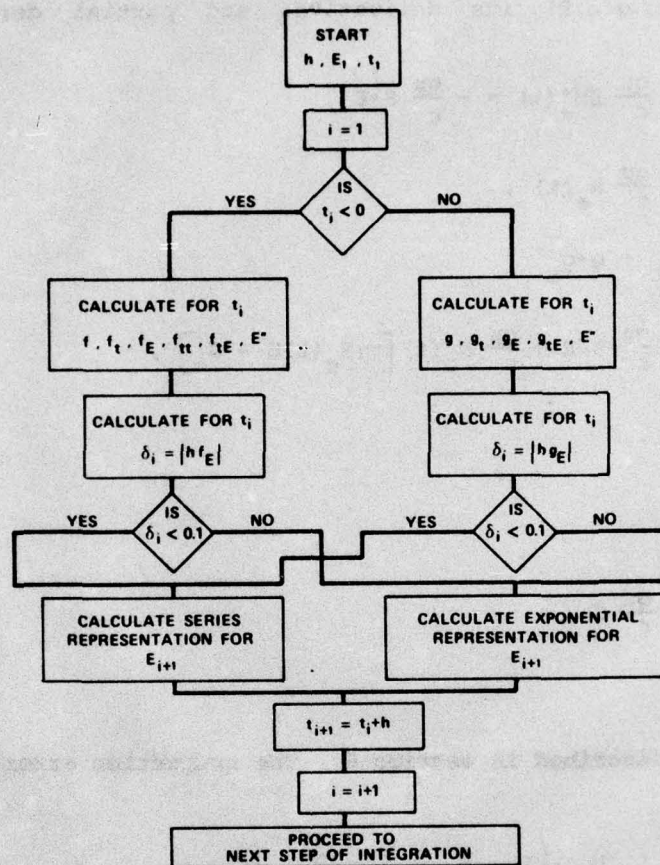


Figure 2. Exponential Differencing Method.



## 6. NUMERICAL VALUES

Finding the solution of equations (1) and (2) required the use of the same hypothetical numerical values as applied by Wyatt<sup>1</sup> for the various constant parameters. These values are as follows:

$$q = 1.6 \cdot 10^{-19} \text{ C},$$

$$N_e(0) = 1.133 \cdot 10^{11} / \text{cm}^3,$$

$$\mu = 2.0 \text{ m}^2/\text{V/s},$$

$$J_c(t) = 1.34 \cdot 10^3 \text{ A/m}^2 \text{ for all } t,$$

$$\epsilon = 8.85 \cdot 10^{-2} \text{ F/m},$$

$$r = 5.0 \cdot 10^8 / \text{s},$$

$$E(0) = 3.697 \cdot 10^4 \text{ V/m}.$$

The free-electron density,  $N_e(t)$ , is given by

$$N_e(t) = N_e(0) + St, \quad (6)$$

where  $t$  is the time and  $S$  is the rate of production of ion pairs per unit volume and is given the value

$$S = 5.664 \cdot 10^{25} / \text{m}^3/\text{s}.$$

Since equation (6) is valid for methane only to 9 ns, any solutions for times beyond this were not possible to calculate. However, it was possible to obtain excellent results and make some interesting comparisons for this restrictive time frame, which are shown in section 7.

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<sup>1</sup>W. T. Wyatt, Internal EMP Strength and Time Dependence for an Idealized Problem, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

## 7. RESULTS AND COMPARISONS

Two computer codes were written to solve differential equations (1) and (2). Computer code HAMMING was written to solve the equations by Hamming's method, and the code EXPDIFF was used to solve the equations by the exponential differencing methods. The listings of HAMMING and EXPDIFF are in appendices A and B, respectively.

Although the solutions from HAMMING compare favorably with the results of Wyatt,<sup>1</sup> the solutions obtained are considered more accurate, since truncation errors are calculated and examined. In table I, specific values from Wyatt<sup>1</sup> and HAMMING are listed to show the agreement of the results. Regarding these results, numerous computer runs were

TABLE I. RESULTS OF ORIGINAL AND HAMMING

Time (s)	Original Electric field strength (V/m)	HAMMING Electric field strength ( $\Delta t = 1.0 \cdot 10^{-12}$ ) (V/m)
$-4.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6970 \cdot 10^4$
$-3.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6965 \cdot 10^4$
$-2.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6961 \cdot 10^4$
$-1.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6960 \cdot 10^4$
0	$3.80 \cdot 10^4$	$3.6959 \cdot 10^4$
$5.0 \cdot 10^{-10}$	$3.00 \cdot 10^4$	$3.2129 \cdot 10^4$
$1.0 \cdot 10^{-9}$	$2.48 \cdot 10^4$	$2.6259 \cdot 10^4$
$1.5 \cdot 10^{-9}$	$2.10 \cdot 10^4$	$2.2092 \cdot 10^4$
$2.0 \cdot 10^{-9}$	$1.85 \cdot 10^4$	$1.9107 \cdot 10^4$
$3.0 \cdot 10^{-9}$	$1.47 \cdot 10^4$	$1.5093 \cdot 10^4$
$4.0 \cdot 10^{-9}$	$1.20 \cdot 10^4$	$1.2496 \cdot 10^4$
$5.0 \cdot 10^{-9}$	$1.00 \cdot 10^4$	$1.0670 \cdot 10^4$
$6.0 \cdot 10^{-9}$	$8.80 \cdot 10^3$	$9.3132 \cdot 10^3$
$7.0 \cdot 10^{-9}$	$8.00 \cdot 10^3$	$8.2648 \cdot 10^3$
$8.0 \cdot 10^{-9}$	$7.40 \cdot 10^3$	$7.4296 \cdot 10^3$
$9.0 \cdot 10^{-9}$	$7.00 \cdot 10^3$	$6.7483 \cdot 10^3$

<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).



made with different time step sizes, which revealed some interesting facts. When the time step size  $\Delta t = 1.0 \cdot 10^{-10}$  was used, stability of the solution was obtained from 0 to approximately 6.5 ns, while from 6 to 9 ns, the solution became dominated by very large truncation errors and, thus, resulted in an unstable solution over this time frame. Using the time step sizes  $\Delta t = 1.0 \cdot 10^{-11}$  and  $\Delta t = 1.0 \cdot 10^{-12}$  did not produce any stability problems during the time frame 0 to 9 ns, and the truncation errors were considerably smaller than for  $\Delta t = 1.0 \cdot 10^{-10}$ . The truncation errors did not decrease, however, when the time step size was lowered to  $\Delta t = 1.0 \cdot 10^{-13}$ , as they remained approximately on the same order of magnitude. An example of these results appears in table II.

TABLE II. HAMMING'S TRUNCATION ERRORS FOR DIFFERENT TIME STEP SIZES

Time (s)	Truncation errors for time step sizes ( $\Delta t$ )			
	$\Delta t = 1.0 \cdot 10^{-10}$	$\Delta t = 1.0 \cdot 10^{-11}$	$\Delta t = 1.0 \cdot 10^{-12}$	$\Delta t = 1.0 \cdot 10^{-13}$
0	0	0	0	0
$1.0 \cdot 10^{-10}$	0	$3.4909 \cdot 10^{-6}$	$-8.6590 \cdot 10^{-11}$	$-1.2123 \cdot 10^{-10}$
$2.0 \cdot 10^{-10}$	0	$4.1106 \cdot 10^{-6}$	$-1.7318 \cdot 10^{-11}$	$-6.9272 \cdot 10^{-11}$
$3.0 \cdot 10^{-10}$	0	$4.0913 \cdot 10^{-6}$	$-5.1954 \cdot 10^{-11}$	$-1.2123 \cdot 10^{-10}$
$4.0 \cdot 10^{-10}$	$1.9735 \cdot 10^{-1}$	$3.6824 \cdot 10^{-6}$	$-6.9272 \cdot 10^{-11}$	$-1.3854 \cdot 10^{-10}$
$1.0 \cdot 10^{-9}$	$8.5146 \cdot 10^{-2}$	$5.5282 \cdot 10^{-7}$	$-6.9272 \cdot 10^{-11}$	$-6.0613 \cdot 10^{-11}$
$2.0 \cdot 10^{-9}$	$-1.1649 \cdot 10^{-3}$	$-1.5846 \cdot 10^{-8}$	$-5.1954 \cdot 10^{-11}$	$-4.3295 \cdot 10^{-11}$
$3.0 \cdot 10^{-9}$	$-1.7558 \cdot 10^{-4}$	$-3.2038 \cdot 10^{-9}$	$-6.4942 \cdot 10^{-11}$	$-5.1954 \cdot 10^{-11}$
$4.0 \cdot 10^{-9}$	$-1.0871 \cdot 10^{-4}$	$-8.9188 \cdot 10^{-10}$	$-3.8965 \cdot 10^{-11}$	$-2.5977 \cdot 10^{-11}$
$5.0 \cdot 10^{-9}$	$-8.4018 \cdot 10^{-3}$	$-3.4203 \cdot 10^{-10}$	$-2.1647 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$6.0 \cdot 10^{-9}$	$-1.2692 \cdot 10^1$	$-1.6019 \cdot 10^{-10}$	$-3.0306 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$7.0 \cdot 10^{-9}$	$-2.3989 \cdot 10^5$	$-8.6590 \cdot 10^{-11}$	$-3.4636 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$8.0 \cdot 10^{-9}$	$-5.0072 \cdot 10^{10}$	$-6.4942 \cdot 10^{-11}$	$-1.9483 \cdot 10^{-11}$	$-2.1647 \cdot 10^{-11}$
$9.0 \cdot 10^{-9}$	$-9.8303 \cdot 10^{16}$	$-3.2471 \cdot 10^{-11}$	$-1.2988 \cdot 10^{-11}$	$-1.0824 \cdot 10^{-11}$

Some interesting occurrences were noted when analyzing the results of EXPDIFF. First, EXPDIFF was very simple to code. In fact, because of the relative ease and simplicity in programming EXPDIFF, valid results were obtained on the first computer run. Second, the results of EXPDIFF were quite favorable when compared to the results obtained by Wyatt<sup>1</sup> and again are considered more accurate because of the calculation

<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

TABLE III. RESULTS OF ORIGINAL, HAMMING, AND EXPDIFF

Time (s)	Original Electric field strength (V/m)	HAMMING Electric field strength $\Delta t = 1.0 \cdot 10^{-12}$ (V/m)	EXPDIFF Electric field strength $\Delta t = 1.0 \cdot 10^{-12}$ (V/m)
$-4.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6970 \cdot 10^4$	$3.6970 \cdot 10^4$
$-3.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6965 \cdot 10^4$	$3.6965 \cdot 10^4$
$-2.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6961 \cdot 10^4$	$3.6961 \cdot 10^4$
$-1.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6960 \cdot 10^4$	$3.6960 \cdot 10^4$
0	$3.80 \cdot 10^4$	$3.6959 \cdot 10^4$	$3.6959 \cdot 10^4$
$5.0 \cdot 10^{-10}$	$3.00 \cdot 10^4$	$3.2129 \cdot 10^4$	$3.2135 \cdot 10^4$
$1.0 \cdot 10^{-9}$	$2.48 \cdot 10^4$	$2.6259 \cdot 10^4$	$2.6264 \cdot 10^4$
$1.5 \cdot 10^{-9}$	$2.10 \cdot 10^4$	$2.2092 \cdot 10^4$	$2.2095 \cdot 10^4$
$2.0 \cdot 10^{-9}$	$1.85 \cdot 10^4$	$1.9107 \cdot 10^4$	$1.9110 \cdot 10^4$
$3.0 \cdot 10^{-9}$	$1.47 \cdot 10^4$	$1.5093 \cdot 10^4$	$1.5094 \cdot 10^4$
$4.0 \cdot 10^{-9}$	$1.20 \cdot 10^4$	$1.2496 \cdot 10^4$	$1.2497 \cdot 10^4$
$5.0 \cdot 10^{-9}$	$1.00 \cdot 10^4$	$1.0670 \cdot 10^4$	$1.0670 \cdot 10^4$
$6.0 \cdot 10^{-9}$	$8.80 \cdot 10^3$	$9.3132 \cdot 10^3$	$9.3138 \cdot 10^3$
$7.0 \cdot 10^{-9}$	$8.00 \cdot 10^3$	$8.2648 \cdot 10^3$	$8.2652 \cdot 10^3$
$8.0 \cdot 10^{-9}$	$7.40 \cdot 10^3$	$7.4296 \cdot 10^3$	$7.4299 \cdot 10^3$
$9.0 \cdot 10^{-9}$	$7.00 \cdot 10^3$	$6.7483 \cdot 10^3$	$6.7486 \cdot 10^3$

and analysis of the truncation errors (table III). Probably the most significant aspect of EXPDIFF was the results of comparisons with HAMMING.

In comparing the codes, several significant points of interest were revealed. There was a noticeable ease in the programming of EXPDIFF compared with the more difficult effort required for HAMMING. In fact, a very generous analysis of this coding effort was that HAMMING took at least twice as long to code as EXPDIFF. Although HAMMING is generally considered to give more accurate calculations, EXPDIFF yielded results that were extremely close (sometimes exact) to the solutions obtained from HAMMING (table III). However, the most significant result was the stability of EXPDIFF when compared with HAMMING. For the time step size  $\Delta t = 1.0 \cdot 10^{-11}$ , the truncation errors were approximately the same size, except in several cases where truncation errors from HAMMING were



an order of magnitude smaller. When the time step size was increased to  $\Delta t = 1.0 \cdot 10^{-10}$ , HAMMING became unstable at about 6.5 ns, while EXPDIFF yielded truncation errors on the order of  $10^{-6}$  for 0 to 9 ns. This timing is illustrated in table IV. An even more meaningful result was noticed when considering the large step size of  $\Delta t = 1.0 \cdot 10^{-9}$ . For this step size, EXPDIFF was stable through 9 ns, since truncation errors on the order of  $10^{-2}$  were tolerated. Whereas EXPDIFF exhibited reasonable truncation errors for this step size, HAMMING, as expected, became dominated by the buildup of truncation errors and, thus, was unstable. The truncation errors of EXPDIFF for  $\Delta t = 1.0 \cdot 10^{-9}$  can be seen in table V.

TABLE IV. TRUNCATION ERRORS FOR DIFFERENT TIME STEP SIZES FOR HAMMING AND EXPDIFF

Time (s)	Truncation errors at time step size $1.0 \cdot 10^{-10}$		Truncation errors at time step size $1.0 \cdot 10^{-11}$	
	HAMMING	EXPDIFF	HAMMING	EXPDIFF
0	0	$7.4679 \cdot 10^{-5}$	0	$5.0168 \cdot 10^{-8}$
$1.0 \cdot 10^{-10}$	0	$5.9718 \cdot 10^{-11}$	$3.4909 \cdot 10^{-6}$	$3.9421 \cdot 10^{-9}$
$2.0 \cdot 10^{-10}$	0	$5.1673 \cdot 10^{-6}$	$4.1106 \cdot 10^{-6}$	$6.740 \cdot 10^{-9}$
$3.0 \cdot 10^{-10}$	0	$8.4422 \cdot 10^{-6}$	$4.0913 \cdot 10^{-6}$	$8.3.3 \cdot 10^{-9}$
$4.0 \cdot 10^{-10}$	$1.9735 \cdot 10^{-1}$	$1.0322 \cdot 10^{-5}$	$3.6824 \cdot 10^{-6}$	$9.0334 \cdot 10^{-9}$
$1.0 \cdot 10^{-9}$	$8.5146 \cdot 10^{-2}$	$9.7018 \cdot 10^{-6}$	$5.5282 \cdot 10^{-7}$	$7.0506 \cdot 10^{-9}$
$2.0 \cdot 10^{-9}$	$-1.1649 \cdot 10^{-3}$	$5.3903 \cdot 10^{-6}$	$-1.5846 \cdot 10^{-8}$	$3.6655 \cdot 10^{-9}$
$3.0 \cdot 10^{-9}$	$-1.7558 \cdot 10^{-4}$	$3.5640 \cdot 10^{-6}$	$-3.2038 \cdot 10^{-9}$	$2.2718 \cdot 10^{-9}$
$4.0 \cdot 10^{-9}$	$-1.0871 \cdot 10^{-4}$	$2.6160 \cdot 10^{-6}$	$-8.9188 \cdot 10^{-10}$	$1.5602 \cdot 10^{-9}$
$5.0 \cdot 10^{-9}$	$-8.4018 \cdot 10^{-3}$	$2.0477 \cdot 10^{-6}$	$-3.4203 \cdot 10^{-10}$	$1.1436 \cdot 10^{-9}$
$6.0 \cdot 10^{-9}$	$-1.2692 \cdot 10^1$	$1.6749 \cdot 10^{-6}$	$-1.6019 \cdot 10^{-10}$	$8.7743 \cdot 10^{-10}$
$7.0 \cdot 10^{-9}$	$-2.3989 \cdot 10^5$	$1.4142 \cdot 10^{-6}$	$-8.6590 \cdot 10^{-11}$	$6.9648 \cdot 10^{-10}$
$8.0 \cdot 10^{-9}$	$-5.0072 \cdot 10^{10}$	$1.2230 \cdot 10^{-6}$	$-6.4942 \cdot 10^{-11}$	$5.6760 \cdot 10^{-10}$
$9.0 \cdot 10^{-9}$	$-9.8303 \cdot 10^{16}$	$1.0775 \cdot 10^{-6}$	$-3.2471 \cdot 10^{-11}$	$4.7242 \cdot 10^{-10}$

TABLE V. EXPDIFF TRUNCATION ERRORS AT TIME STEP SIZE  $1.0 \cdot 10^{-9}$

Time (s)	Truncation errors
0	$8.7131 \cdot 10^{-1}$
$1.0 \cdot 10^{-9}$	$2.1944 \cdot 10^{-7}$
$2.0 \cdot 10^{-9}$	$5.1673 \cdot 10^{-2}$
$3.0 \cdot 10^{-9}$	$3.4598 \cdot 10^{-2}$
$4.0 \cdot 10^{-9}$	$2.5851 \cdot 10^{-2}$
$5.0 \cdot 10^{-9}$	$2.0672 \cdot 10^{-2}$
$6.0 \cdot 10^{-9}$	$1.7226 \cdot 10^{-2}$
$7.0 \cdot 10^{-9}$	$1.4766 \cdot 10^{-2}$
$8.0 \cdot 10^{-9}$	$1.2920 \cdot 10^{-2}$
$9.0 \cdot 10^{-9}$	$1.1484 \cdot 10^{-2}$

## 8. CONCLUSIONS

With regard to the comparisons made between the predictor-corrector routine HAMMING and the exponential differencing method EXPDIFF, there seem to be two compelling factors that make the exponential differencing technique superior. First, the ease and simplicity of the programming effort required for EXPDIFF far outweigh the more complicated coding work needed for HAMMING. Second and probably more important, the stability properties of EXPDIFF are excellent, whereas the solutions calculated by HAMMING became dominated by truncation errors during the time frame examined for particular time step sizes. This stability property is best exemplified by the large step size ( $1.0 \cdot 10^{-9}$ ) that can be used with relative assuredness of accurate results. Thus, this stability factor represented by the reasonable truncation errors of EXPDIFF far outweigh the somewhat smaller truncation errors of HAMMING. Therefore, considering the ease of programming and the stability properties, the exponential differencing method provides an efficient and reliable solution to the differential equations involved in this EMP problem and is strongly recommended for solving other differential equations of this type.



# SYMBOLS

$E(t)$	Electric-field strength
$\epsilon$	Permittivity of free space
$J_c(t)$	Compton electron current density
$\mu$	Electron mobility
$N_e(t)$	Free electron density
$q$	Electronic charge
$r$	Model parameter for gamma flux rate history
$s$	Rate of production of ion pairs per unit volume
$t$	Time

**APPENDIX A.--COMPUTER CODE HAMMING**

**This appendix contains a complete listing of HAMMING.**



PROGRAM HANNING 74/74 OPT=1 FTM 4.5+14 06/04/76 13.30.02 PAGE 1

```

1  PROGRAM HANNING(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
   INTEGER FLAG
   REAL NORD(10),MABS(10)
   COMMON/A/E(5000),M(5000),EP(5000),DEL,START,ESTART
5  COMMON/B/VAL(5000),CF(5000)
   COMMON/C/RNE(5000),SRE(5000)
   DIMENSION N(5000),TITLE(20)
   DIMENSION ERROR(5000)
   DIMENSION TERR(5000)
   DIMENSION ECOREC(60),ECORECP(60)
10  L=1
   IT=0
   READ(5,20)DEL,TMAX,EP5LOM,START,ESTART,M
15  FORMAT(5E10.3,15)
   CF(1)=EP5LOM
   C  CALCULATE STARTING VALUES Y1,Y2,Y3,USING RUNGE-KUTTA TECHNIQUE
   C
   CALL RUNGE
   DO 30 J=1,4
   CF(J)=EP5LOM
30  EP(J)=FET(M(J),E(J),J)
   I=4
   C  PREDICT Y(N+1) USING MILNE'S PREDICTOR
   C
40  CALL PREDICT(I,EPDIP)
   CF(I+1)=EP5LOM
   MIT(I)=M(I)+DEL
   EPDIP=FET(M(I+1),EPDIP,0)
   ECOREC(I)=EPDIP
   ECORECP(I)=EPDIP
   C  CORRECT Y(N+1) USING HANNING'S CORRECTOR
   C
35  C  CALL CORRECT(I,ECORECP(I),ECOREC(I+1))
   ECORECP(I+1)=FET(M(I+1),ECOREC(I),0)
   IF(L.EQ.1) GO TO 55
   C  CHECK TO SEE IF ERROR RESULTS FROM NOT ITERATING TO CONVERGENCE
   C
45  CALL ERROR(I,L,EPDIP,ECOREC(I),ECOREC(I+1),ECORECP(I),
   ECORECP(I+1),FLAG,IT)
   IF(FLAG) 53,60,60
53  ERROR(I+1)=ABS(ECORECP(I+1)-ECOREC(I))
55  L=L+1
   GO TO 50
60  K(I+1)=L-1
   C  CALCULATE CORRECT VALUE OF Y(N+1) USING HANNING'S CORRECTOR
   C
55  CALL CORRECT(I,ECORECP(I+1),ECOR)
   E(I+1)=ECOR
   EP(I+1)=FET(MIT(I+1),E(I+1),I+1)
   C  CALCULATE TRUNCATION ERROR

```

# APPENDIX A

PROGRAM NAMING 74/74 OPT-1 PAGE 2 06/04/76 13.30.02 FTA 4.54414

```

C
60      TERR(1:1) = (9./121.) * (E(1:1) - EPD1C)
      N=1:1
      I=1:1
      L=1
      IF (M(1:1, L, TMAX)) GO TO 40
65      WRITE(6,70)
70      FORMAT(1M)
      WRITE(6,80) DEL.TMAX, N, EPSLON, START
      FORMAT(1X, 17HDELTA TIME STEPS, 1PE10.3, 5X,
80      12HMAXIMUM TIME TO BE PLOTTED, 1PE10.3, 5X,
      22HINCREMENT OF OUTPUT VALUES, 15./,
      34H23HCONVERGENCE TOLERANCE, 1PE10.3,
      45H15HSTARTING TIME, 1PE10.3, //, /)
      IF (E(1:1, 50, AND.FLAG.EB.-1)) GO TO 140
      WRITE(6,90)
90      FORMAT(17, /, 53X, 9HNUMBER OF, 10X, 8HERROR BY)
      WRITE(6,100)
100     FORMAT(4X, 4HTIME, 14X, 1ME, 7X, 16HTRUNCATION ERROR, 3X,
      110HCONVERGENCE CYCLES, 3X, 13HNOT ITERATING, 3X,
      210HCONVERGENCE FACTOR, 5X, 6HOLD ME, 8X, 6HNEW ME)
      WRITE(6,110)
110     FORMAT(4X, 4H-----, 14X, 1H, 7X, 16H-----, 3X,
      118H-----, 3X, 13H-----, 8X, 6H-----)
      210H-----
      DO 130 J=1, N, N
      WRITE(6,120) M(J), E(J), TERR(J), K(J), VAL(J), CF(J), RME(J), SNE(J)
120     FORMAT(1X, 3(1PE11.4, 5X), 7X, 13, 11X, 1PE11.4, 8X, 1PE11.4, 7X, 1PE11.4,
      13X, 1PE11.4)
130     CONTINUE
C
90      TITLE(1) = 10HEND TIME D
      TITLE(2) = 10HDEPENDENCY
      TITLE(3) = 5HSTUDY
      TITLE(4) = 1H
      TITLE(5) = 1H
      NORD(1) = 10HELECTRIC F
      NORD(2) = 10HFIELD STRENGTH
      NORD(3) = 10HGT V/N
      NABS(1) = 4HTIME
      NABS(2) = 1H
      NABS(3) = 1H
C
      CALL PLOT(IN, MAX)
      CALL PRPLOT(E, MAX, TITLE, NABS, NORD, 0., 0., 100)
      GO TO 155
140     KL=1:1
150     WRITE(6,150) KL, ERROR(KL)
150     FORMAT(17, /, /, 2X, 6HNOT CONVERGE IN 50 ITERATIONS WHILE CALC.,
155     110HULATING E, 15, 25H) - CONVERGENCE ERROR, 1PE11.4)
160     READ(5,160) IK
160     FORMAT(9X, 11)
      GO TO (10, 170), IK
170     CONTINUE
      END

```



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FTM 4.5+414

PROGRAM NAMING 74/74 OPT-1

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

112 I

## SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS 4111 NAMING	DEF LINE 1	REFERENCES											
VARIABLES	SN	TYPE	RELOCATION										
11A10 CF	REAL	ARRAY B		5	84	DEFINED	15	21	28				
35230 DEL	REAL	ARRAY A		4	29	66	DEFINED	13	104				
O E	REAL	ARRAY A		4	22	55	59	84					
4445 ECR	REAL			54	54								
42352 ECDREC	REAL	ARRAY		REFS									
42246 ECDREC	REAL	ARRAY		REFS									
				REFS									
				DEFINED									
23A20 EP	REAL	ARRAY A		32	37	2442	2445	DEFINED	31				
4443 EPDIP	REAL			4	REFS	22	55						
4444 EPDIP	REAL			27	30	31	42	59					
4437 EPDIP	REAL			32	30	30							
16332 EPRDIP	REAL	ARRAY		15	21	28	66	DEFINED	13				
35232 EPRDIP	REAL	ARRAY		8	107	DEFINED	45						
4833 FLAG	INTEGER	ARRAY A		4	REFS	13	72						
11010 H	REAL	ARRAY A		2	42	44	30						
				REFS	22	29	30	37	55	63			
4442 I	INTEGER			4	REFS	22	29						
				104	DEFINED	29							
4451 IK	INTEGER			REFS	27	28	30	36	37	42			
4435 IT	INTEGER			45	53	54	455	259	60	61			
4441 J	INTEGER			63	DEFINED	23	61						
4476 K	INTEGER			112	DEFINED	110							
4450 KL	INTEGER	ARRAY		REFS	42	12	DEFINED	20	83				
4434 L	INTEGER			21	4022	8084	49						
				REFS	7	84							
				20107	DEFINED	106	2036	38	5042	2045			
				31	32	53	72	DEFINED	11	47			
				46	47								
4440 M	INTEGER			62	REFS	83	13						
4447 MAX	INTEGER			REFS	103	104							
4444 N	INTEGER			REFS	83	103	60						
4444 NAB5	REAL	ARRAY		REFS	3	104	DEFINED	99	100				
4452 NORD	REAL	ARRAY		REFS	3	104	DEFINED	96	57				
O RME	REAL	ARRAY C		REFS	6	84							
11010 SRE	REAL	ARRAY C		REFS	6	84							
35231 START	REAL	ARRAY A		REFS	4	66	DEFINED	13					
30342 TERR	REAL	ARRAY		REFS	9	84	DEFINED	59					
16506 TITLE	REAL	ARRAY		REFS	7	104	DEFINED	90	92	93			
				94									
4436 TMAX	REAL	ARRAY B		REFS	63	64	DEFINED	13					
O VAL	REAL	ARRAY		REFS	5	84							

# APPENDIX A

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FTN 4.54414

OPT=1

74/74

PROGRAM NAMING

FILE NAMES

0 INPUT

2001 OUTPUT

0 TAPES

2001 TAPE4

EXTERNALS

CORRECT

ERROR

FET

PLOT

PREDICT

PRIPLOT

RUNGE

TYPE

REAL

ARGC

1

INTRIN

DEF LINE

REFERENCES

45

STATEMENT LABELS

4112 10

4425 20

0 30

4134 40

4150 50

0 53

4200 55

4202 60

4228 65

4433 70

4445 80

4473 90

4503 100

4524 110

4555 120

0 130

4310 140

4572 150

4316 155

4613 160

4327 170

INDEX

FROM-TO

LENGTH

PROPERTIES

EXT REFS

EXT REFS

EXT REFS

COMMON BLOCKS

LENGTH

MEMBERS - BIAS NAME(LENGTH)

0 E (5000)

1500C DEL (1)

0 VAL (5000)

0 PNE (5000)

STATISTICS

PROGRAM LENGTH

362378 15519

41038 2115

CM LABELED COMMON LENGTH

1042738 35003

5000 H (5000)

15001 START (1)

5000 CF (5000)

5000 SNE (5000)

10000 EP (5000)

15002 ESTART (1)





# APPENDIX A

2

PAGE

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FTN 4.5+414

74/74 OPT=1

SUBROUTINE RUNGE

STATEMENT LABELS

DEF LINE REFERENCES

6 10

6 20

COMMON BLOCKS

LENGTH

MEMBERS - BIAS NAME(LENGTH)

A

15003

O F (5000)

1500C DEL (1)

10000 EP (5000)

15002 ESTART (1)

5000 H (5000)

15001 START (1)

STATISTICS

PROGRAM LENGTH

1146 76

CR LABELED COMMON LENGTH

352338 15003





# APPENDIX A

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FTM 4.5-414

SUBROUTINE CORRECT 74/74 OPT-1

```

1      SUBROUTINE CORRECT(I,EDICP,ECREC)
COMMON/A/(15000),M(15000),EP(15000),DEL,START,ESTART
V1=19,OE(11)-E(11-2))/R.
V2=EDICP+2,EP(11)-E(11-1)
ECREC=V1+113,DEL/0.1072
RETURN
END

```

## SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS DEF LINE REFERENCES

3 CORRECT 1 6

VARIABLES IN TYPE RELOCATION

ADDRESS	NAME	TYPE	RELOCATION	REFS
35230	DEL	REAL	A	REFS
0	E	REAL	A	REFS
0	ECREC	REAL	A	DEFINED
0	EDICP	REAL	F.P.	REFS
23420	EP	REAL	A	REFS
35232	ESTART	REAL	A	REFS
11610	M	REAL	A	REFS
0	I	INTEGER	A	REFS
35231	START	REAL	A	REFS
26	V1	REAL		REFS
27	V2	REAL		REFS

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

0 E (15000)

15000 DEL (1)

5000 M (15000)

15001 START (1)

10000 EP (15000)

15002 ESTART (1)

STATISTICS  
PROGRAM LENGTH 308 24  
CM LABELED COMMON LENGTH 352338 15003



## APPENDIX A

SUBROUTINE FROM 74/74 OPT-1

```

1  SUBROUTINE ERROR(I,L,EPDIC,P,C,PP,CP,FLAG,IT)
COMMON/AF(5000),MF(5000),EP(5000),DEL,START,ESTART
INTEGER FLAG
8=3/8.
10  DELTA=ABS(CP-PP)
    IF(DELTA.LE.CP(I+1)) GO TO 20
    IF(FLAG.JO) GO TO 15
    CF(I+1)=DELTA*CF(I+1)
15  FLAG=-1
    RETURN
20  ARG=C-P
    IF(ARG.EQ.0.) ARG=1.E-5
    RK=DELTA/ABS(ARG)
    VAL(I+1)=(DEL+0.2)*(0+0.2)*DELTA*RK
    CALL CORRECT(I,PP,C)
    EC=C
    ER=1./121./DELTA*(EC-EPDIC)
    IF(VAL(I+1).GT.ABS(ER)) GO TO 40
    FLAG=0
    RETURN
40  IF(I+1)
    IF(17-GT.0) GO TO 80
    WRITE(6,60)
    FORMAT(1H1)
    WRITE(6,70)
    FORMAT(1//,0.1X,40THE ERROR INCURRED BY NOT ITERATING THE
    2//,1X,12HRECTOR TO CONVERGE IS GREATER THAN THE TRUNCATION ERROR.
    3//,1X,12HRECTOR BY NOT//,1X,12HITERATING TO,5X,10HTRUNCATION.
    4//,1X,12H1X,11HCONVERGENCE,1X,5HERROR)
    IT=1
80  WRITE(6,90) IF(VAL(I+1).ERR
90  FORMAT(5X,2HE16,1X,1H15X,1HE11.4,5X,1HE11.4)
    FLAG=1
    RETURN
END

```

## SYMBOLIC REFERENCE MAP (R-3)

[illegible]





# APPENDIX A

SUBROUTINE PLOT 74/74 OPT=1 PAGE 1

```

1 SUBROUTINE PLOT(M,MAX)
COMMON/AL/EP(5000),H(5000),EP(5000),DEL,START,ESTART
RT=H/100.
IDEL=INT(RT)
IF(IDEL.EQ.0) IDEL=1
L=1
DO 10 I=1,M,IDEI
M(I)=M(I)
E(I)=E(I)
L=L+1
10 CONTINUE
MAX=L
RETURN
END

```

## SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS 3 PLOT	DEF LINE 1	REFERENCES 13
VARIABLES	SM	TYPE
35230 DEL	REAL	RELOCATION
0 E	REAL	REFS
29420 EP	REAL	REFS
35232 ESTART	REAL	REFS
11010 H	REAL	REFS
34 I	INTEGER	REFS
32 IDEI	INTEGER	REFS
33 L	INTEGER	REFS
0 MAX	INTEGER	REFS
0 M	INTEGER	REFS
31 RT	REAL	REFS
35231 START	REAL	REFS
INLINE FUNCTIONS	TYPE	ARGS
1 INT	INTEGER	1
DEF LINE REFERENCES	1	INTIN
STATEMENT LABELS	DEF LINE REFERENCES	4
0 10	11	7
LOOP'S LABEL	INDEX	FROM-TO
17 10	1	7 11
COMMON BLOCKS	LENGTH	PROPERTIES
4	15003	INSTACK
MEMBERS - BIAS NAME(LENGTH)	0 E	(5000)
15000 DEL	(1)	
STATISTICS	PROGRAM LENGTH	350
CN LABELED COMMON LENGTH	35230	15003
5000 H	(5000)	
15001 START	(1)	
10000 EP	(5000)	
15002 ESTART	(1)	
9	DEFINED	9
0	DEFINED	0
6	DEFINED	6
7	DEFINED	7
4	DEFINED	4
12	DEFINED	12
10	DEFINED	10
1	DEFINED	1
3	DEFINED	3
4	DEFINED	4
2	DEFINED	2

# APPENDIX A

PAGE 1

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FTN 4.5-414

FUNCTION FET 74/74 OPT=1

```

1      FUNCTION FET(TI,ET,N)
      REAL JC,MUP,ME
      D=5.0E+8
      EPS=8.95E-12
      Q=1.6E-19
      MUP=2.0
      IF(TI-ET-Q.1) GO TO 10
      C ME(T) IS MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
      FET=(JC(TI)-1.E+6*ME(TI,N))*MUP*ET*EXP(R*OTI))/EPS
      RETURN
10      C ME(T) IS MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
      FET=(JC(TI)-1.E+6*ME(TI,N))*MUP*ETI/EPS
      RETURN
      END

```

## SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	13
4 FET	1	10	
VARIABLES	SM	TYPE	RELOCATION
73 EPS	REAL		
0 ET	REAL		
70 FET	REAL		
0 K	INTEGER		
71 MUP	REAL		
74 Q	REAL		
72 R	REAL		
0 TI	REAL		
EXTERNALS	TYPE	ARGS	REFERENCES
EXP	REAL	1 LIBRARY	9
JC	REAL	1	2
ME	REAL	2	2
STATEMENT LABELS		DEF LINE	REFERENCES
36 10		12	7
STATISTICS			
PROGRAM LENGTH		758	61



# APPENDIX A

PAGE 1

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FTM 4.5+414

74/74 OPT-1

FUNCTION NE

```

1 REAL FUNCTION NEIT(K)
COMMON/C/RNE(1000),SNE(1000)
REAL RNE
RNE=1.133E+11
S=5.664E+19
IF (T.GE.0.) GO TO 10
RNE=1.133E+11
RNE(K)=0.
SNE(K)=0.
RETURN
10 RNE=NEO+S*T
IF (R.EQ.0) RETURN
SNE(K)=RNE
RNEO=1.133E+11
R5=1.022E+20
DELTA=1.0008E+8
A=4.E-7
ARG=R*RS*(T+2)
X=5*ARG
Y=DELTA*T
Z=X-Y
F1=R5/(2.*DELTA)
F2=1.*EXP(X)
F3=EXP(Y)-1.
F4=EXP(Z)
RNE(K)=(F1+F2+F3+RNEO)*F4
RETURN
END

```

## SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	12	27
4 NE	1	10		
VARIABLES	SM	TYPE	RELOCATION	
70 A	REAL			REFS
71 ARG	REAL			REFS
67 DELTA	REAL			REFS
75 F1	REAL			REFS
76 F2	REAL			REFS
77 F3	REAL			REFS
100 F4	REAL			REFS
0 K	INTEGER			REFS
62 NE	REAL		F.P.	DEFINED
63 NEO	REAL			REFS
0 RNE	REAL			REFS
A5 RNEO	REAL	ARRAY	C	REFS
66 RS	REAL			REFS
64 S	REAL			REFS
1010 SNE	REAL	ARRAY	C	REFS
0 T	REAL		F.P.	REFS
72 X	REAL			REFS

10	DEFINED	17	DEFINED	10	DEFINED	16
19	DEFINED	18	DEFINED	20	DEFINED	
20	DEFINED	22	DEFINED	21	DEFINED	
26	DEFINED	23	DEFINED	26	DEFINED	
26	DEFINED	24	DEFINED	26	DEFINED	
26	DEFINED	25	DEFINED	26	DEFINED	
8	DEFINED	9	DEFINED	8	DEFINED	
13	DEFINED	7	DEFINED	13	DEFINED	
3	DEFINED	11	DEFINED	3	DEFINED	
2	DEFINED	8	DEFINED	2	DEFINED	
26	DEFINED	14	DEFINED	26	DEFINED	
10	DEFINED	22	DEFINED	10	DEFINED	
11	DEFINED	5	DEFINED	11	DEFINED	
2	DEFINED	9	DEFINED	2	DEFINED	
4	DEFINED	11	DEFINED	4	DEFINED	
21	DEFINED	23	DEFINED	21	DEFINED	

DEFINED 1

# APPENDIX A

PAGE 2

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FTN 4.54414

74/74 OPT=1

VARIABLES SM TYPE RELOCATION  
 73 V REAL  
 74 Z REAL

21 24 DEFINED 20  
 25 DEFINED 21

REFS  
REFS

EXTERNALS TYPE  
 END REAL

25

ARGUMENTS  
 1 LIBRARY 23 24

STATEMENT LABELS  
 15 10

DEF LINE REFERENCES  
 11 6

COMMON BLOCKS LENGTH  
 C 10000

5000 SNE (5000)

STATISTICS  
 PROGRAM LENGTH 1018 65  
 CM LABELED COMMON LENGTH 234208 10000



```

1  REAL FUNCTION JC17)
2  R=5.E+0
3  IF(Y.GT.0.) GO TO 10
4  JC=1.34E+3*EXP(M*Y)
5  RETURN
6  10 JC=1.34E+3
7  RETURN
8  END

```

[illegible]

# APPENDIX A

PAGE 1

10/27/76 09.31.03

FTN 4.64420

SUBROUTINE PRTPLOT 74/74 OPT=1

```

1      C      SUBROUTINE PRTPLOT (HORZ,VERT,NPTS,HEAD,MLAB,VLAB,MREF,VREF,J)
      C      THIS FORTRAN SUBROUTINE PRODUCES A FULL PAGE X-Y PRINTER PLOT.
      C
      C      HURZ - REAL ARRAY TO BE PLOTTED ALONG HORIZONTAL AXIS.
      C      VERT - REAL ARRAY TO BE PLOTTED ALONG VERTICAL AXIS.
      C      NPTS - NUMBER OF VALUES IN HORZ,VERT (NTE 101)
      C      HEAD - PLOT HEADING (MUST BE 5 WORDS)
      C      MLAB - LABEL FOR HORIZONTAL AXIS (MUST BE 3 WORDS)
      C      VLAB - LABEL FOR VERTICAL AXIS (MUST BE 3 WORDS)
      C      MREF - REFERENCE VALUE FOR HORIZONTAL AXIS.
      C      VREF - REFERENCE VALUE FOR VERTICAL AXIS.
      C      J - THIS DETERMINES THE SIZE OF THE ARRAYS HORZ AND VERT--NTE 100
      C
15     DIMENSION HORZ(J),VERT(J),HEAD(5),MLAB(3),VLAB(3),LINE(101),
      C IVER(101),JHOR(101),HORIZ(101),VERTIC(101),YAXIS(30),DOUNT(21)
      C INTEGER BLANK,STAR,DOT,EYE
      C
      C      DATA BLANK/1H /,STAR/1H*,DOT/1H./,MINUS/1H-/ ,EYE/1H/
      C
      C      CALL DATE(1DAY)
      C      CALL TIME(1TIM)
      C      HEAD(4)=DAT
      C      HEAD(5)=TIM
      C      MD = 1
      C      NUN = 1
      C      N = NPTS
      C      DE 10 J = 1,N
      C      HORIZ(1) = HORZ(1)
      C      VERTIC(1) = VERT(1)
      C      10 CONTINUE
      C
      C      DECODE (30,1000,VLAB(1)) (YAXIS(1),1-1,30)
      C      1000 FORMAT(30A1)
      C      20 NA = N - 1
      C      DO 30 I = 1,NA
      C      IF (VERTIC(I).GE.VERTIC(I+1)) GO TO 30
      C      HOLD = VERTIC(I)
      C      VERTIC(I) = VERTIC(I+1)
      C      VERTIC(I+1) = HOLD
      C      SAVE = HORIZ(I)
      C      HORIZ(I) = HORIZ(I+1)
      C      HORIZ(I+1) = SAVE
      C      30 CONTINUE
      C      DO 40 J = 1,NA
      C      IF (VERTIC(J).LT.VERTIC(J+1)) GO TO 20
      C      40 CONTINUE
      C      VMAX = VERTIC(1)
      C      VMIN = VERTIC(N)
      C      HMAX = HORIZ(1)
      C      HMIN = HORIZ(N)
      C      DO 50 I = 2,N
      C

```



```

55      HZ = HORIZ(I)
      HMAX = AMAX1(HMAX,HZ)
      HMIN = AMIN1(HMIN,HZ)
      50 CONTINUE
      DO 60 I = 1,N
      JVER = 50.0*(VERTIC(I)-VMIN)/(VMAX-VMIN) + 1.5
      IVER(I) = 52 - JVER
      60 JHOR(I) = 100.0*(HORIZ(I)-HMIN)/(HMAX-HMIN) + 1.5
      KHREF = 100.0*(HREF-VMIN)/(HMAX-VMIN) + 1.5
      IF (KHREF-1.1) KHREF = 150
      IF (KHREF-1.1) KHREF = 150
      IF (KHREF-1.1) KHREF = 150
      KVREF = 50.0*(VREF-VMIN)/(VMAX-VMIN) + 1.5
      KVREF = 52 - KVREF
      IF (KVREF-1.1) KVREF = 1
      IF (KVREF-1.1) KVREF = 1
      UP = (VMAX-VMIN)/50.
      PRINT 200, HEAD
      200 FORMAT(1H1,35X,SA10//)
      DO 200 K = 1,51
      LINE(I) = EYE
      LINE(I) = EYE
      LINE(I) = EYE
      DO 70 I = 2,100
      70 LINE(I) = BLANK
      IF (K-1.1) GO TO 90
      IF (K-1.1) GO TO 90
      IF (K-1.1) GO TO 90
      IF (K-1.1) GO TO 120
      DO 80 I = 2,100
      80 LINE(I) = DOT
      GO TO 120
      90 DO 100 I = 2,100
      100 LINE(I) = MINUS
      DO 110 I = 6,100,5
      110 LINE(I) = EYE
      GO TO 130
      120 IF (KHREF-1.1) GO TO 130
      IF (KHREF-1.1) GO TO 130
      LINE(KHREF) = DOT
      130 IF (K-1.1) GO TO 140
      IF (K-1.1) GO TO 160
      NUM = NUM + 1
      GO TO 150
      140 IF (JHOR(NUM)-1.1) GO TO 150
      IF (JHOR(NUM)-1.1) GO TO 150
      JH = JHOR(NUM)
      LINE(JH) = STAR
      150 NUMBER = NUM + 1
      IF (IVER(NUM)-1.1) GO TO 160
      NUM = NUMBER
      GO TO 140
      160 I = K - 1
      UPT = VMAX - T*UP
      IF (K-1.1) GO TO 170
      IF (K-1.1) GO TO 170

```

# APPENDIX A

PAGE 3

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FTN 4.6-620

SUBROUTINE PATPLT 74/74 DPT-1

```

110 TAXIS = VAXIS(NQ)
    MQ = MQ + 1
    PRINT 3000, TAXIS, UPT, LINE
    3000 FORMAT(1X, A1, 4X, IPE9, 2, 2X, 101A1)
    GO TO 200
170 PRINT 4000, UPT, LINE
    4000 FORMAT(1X, IPE9, 2, 2X, 101A1)
200 CONTINUE
    DLN = (HMAX - HMIN) / 20.
    T = HMIN
    DO 210 I = 1, 21
        DOWN(I) = T
        T = T + DOWN
210 CONTINUE
    PRINT 5000, (DOWN(I), I = 1, 21, 2)
    5000 FORMAT(15X, 1P10E10.2)
    PRINT 6000, (DOWN(I), I = 2, 20, 2)
    6000 FORMAT(20X, 1P10E10.2)
    PRINT 7000, HLAB
    7000 FORMAT(150X, 3A10)
    RETURN
    END

```



**APPENDIX B.--COMPUTER CODE EXPDIFF**

**This appendix contains a complete listing of EXPDIFF.**

PAGE 1

06/04/76 13.30.36

FTN 4.5+014

PROGRAM EXPDIFF 76/74 OPT=1

```

1  PROGRAM EXPDIFF (INPUT, OUTPUT, TAPES-INPUT, TAPES-OUTPUT)
   REAL JC, MU, ME, MORD(3), MABS(3)
   COMMON /A/R, EPS, G, MU, S
   COMMON /B/T(15000), E(15000), DELTA(15000), TERR(15000)
   DIMENSION TITLE(15)
   S=5.664E+19
   R=5.0E+8
   EPS=9.05E-12
   G=1.4E-19
   MU=2.0
10  CONTINUE
   I=1
   READ(5,20) DEL, TSTART, TMAX, ESTART, N, J
20  FORMAT(4E10.3, 15, 15)
   T(1)=TSTART
   E(1)=ESTART
   TERR(1)=0.
   IF(J.NE.1) GO TO 30
   T(1)=T(0)
   E(1)=E(0)
   TSTART=T(1)
   ESTART=E(1)
30  CONTINUE
   IF(T(1)-GT.TMAX) GO TO 70
   IF(T(1)-GE.0.) GO TO 50
   CALL FCALC(1,F,FT,FE,FTT,FTE)
   EDP=FT+FFE
   DELTA(1)=ABS(DELOFE)
   IF(DELTAT(1).LT..1) GO TO 40
   X=EXP(DELOFE)-1.-DELOFE
   E(1)=E(1)+DELOF+EDP*(FE-21)*X
   TERR(1)=1-(DELOF+EDP*(FTT+2.06*FTE))/6.
   T(1)=T(1)+DEL
   I=I+1
   GO TO 30
40  S1=(DELOF+2)/2.
   S2=(DELOF+3)*FE/6.
   S3=(DELOF+4)*(FE+21)/24.
   E(1)=E(1)+DELOF+EDP*(S1+S2+S3)
   TERR(1)=1-(DELOF+3)*(FTT+2.06*FTE)/6.
   T(1)=T(1)+DEL
   I=I+1
   GO TO 30
50  CALL GCALC(1,G,GT,GE,GTE)
   EDP=GT+GGE
   DELTA(1)=ABS(DELOGE)
   IF(DELTAT(1).LT..1) GO TO 60
   X=EXP(DELOGE)-1.-DELOGE
   E(1)=E(1)+DELOG+EDP*(GE-21)*X
   TERR(1)=1-(DELOF+3)*(2.06*GTE)/6.
   T(1)=T(1)+DEL
   I=I+1
   GO TO 30
60  S1=(DELOF+2)/2.
   S2=(DELOF+3)*GE/6.
   S3=(DELOF+4)*(GE+21)/24.
   E(1)=E(1)+DELOG+EDP*(S1+S2+S3)

```



# APPENDIX B

PAGE 2

06/04/76 13.30.36

FTN 4.5+414

PROGRAM EXPDIFF 74/74 OPT-1

```

60      TEND(1:1)=(DEL*0.3)*(2.0*CTE)/6.
        T(1:1)=T(1:1)+DEL
        I=I+1
        GO TO 30
70      CONTINUE
        N=N+1
        CALL OTMRT(M,DEL,ISTART,TRAX)

        TITLE(1:1)=10HNP TIME D
        TITLE(2:1)=10HDEPENDENCY
        TITLE(3:1)=5HSTUDY
        TITLE(4:1)=1M
        TITLE(5:1)=1M
        NORD(1:1)=10HELECTRIC F
        NORD(2:1)=10HFIELD STREN
        NORD(3:1)=10HCTH V/M
        NARS(1:1)=10HTIME
        NARS(2:1)=1M
        NARS(3:1)=1M

        C
        CALL PLOT(M,MAX)
        CALL PRPLY(T,E,MAX,TITLE,NARS,NORD,O.O..O..100)
        READ(5,90) IK
90      FORMAT(IX,13)
        GO TO (10,90),IK
85      STOP
        END
    
```

## CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

04 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

## SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS 6113 EXPDIFF 1 REFERENCES

VARIABLES 4455 DEL SM TYPE REAL RELOCATION

ENTRY POINTS	DEF LINE	REFERENCES	REFS	20	200	31	32	33	36	37
6113 EXPDIFF	1		30	30	40	41	46	200	49	50
4455 DEL	REAL		51	54	55	56	57	58	59	64
25420 DELTA	REAL	ARRAY B	DEFINED	13						
11610 E	REAL	ARRAY B	REFS	4	29	47	DEFINED	28	46	
4471 EDP	REAL		REFS	4	20	22	31	39	49	57
1 EPS	REAL		01	16	16	20	31	39	49	57
4460 ESTART	REAL	A	DEFINED	31	39	49	57	DEFINED	27	45
			REFS	3	DEFINED	8				
			REFS	16	DEFINED	13	22			

# APPENDIX B

PROGRAM EXPDIFF	76/74	DPT-1	RELOCATION	FTN 4.5-414	06/04/76	13.30.36	PAGE	3
<b>VARIABLES</b>	<b>SN</b>	<b>TYPE</b>						
4464 F	REAL			26	31	32	39	40
4465 PE	REAL			26	28	2030	31	37
4466 PT	REAL			26	40			
4467 PTE	REAL			26	40			
4468 PTT	REAL			26	40			
4469 C	REAL			26	45	50	57	58
4470 CE	REAL			26	45	2044	49	55
4471 GTE	REAL			26	58			
4472 I	INTEGER			26	58			
4473 I	INTEGER			26	58			
4474 J	INTEGER			26	58			
4475 K	INTEGER			26	58			
4476 L	INTEGER			26	58			
4477 M	INTEGER			26	58			
4478 N	INTEGER			26	58			
4479 O	INTEGER			26	58			
4480 P	INTEGER			26	58			
4481 Q	INTEGER			26	58			
4482 R	INTEGER			26	58			
4483 S	INTEGER			26	58			
4484 T	INTEGER			26	58			
4485 U	INTEGER			26	58			
4486 V	INTEGER			26	58			
4487 W	INTEGER			26	58			
4488 X	INTEGER			26	58			
4489 Y	INTEGER			26	58			
4490 Z	INTEGER			26	58			
4491 A	REAL			26	58			
4492 B	REAL			26	58			
4493 C	REAL			26	58			
4494 D	REAL			26	58			
4495 E	REAL			26	58			
4496 F	REAL			26	58			
4497 G	REAL			26	58			
4498 H	REAL			26	58			
4499 I	REAL			26	58			
4500 J	REAL			26	58			
4501 K	REAL			26	58			
4502 L	REAL			26	58			
4503 M	REAL			26	58			
4504 N	REAL			26	58			
4505 O	REAL			26	58			
4506 P	REAL			26	58			
4507 Q	REAL			26	58			
4508 R	REAL			26	58			
4509 S	REAL			26	58			
4510 T	REAL			26	58			
4511 U	REAL			26	58			
4512 V	REAL			26	58			
4513 W	REAL			26	58			
4514 X	REAL			26	58			
4515 Y	REAL			26	58			
4516 Z	REAL			26	58			
4517 A	REAL			26	58			
4518 B	REAL			26	58			
4519 C	REAL			26	58			
4520 D	REAL			26	58			
4521 E	REAL			26	58			
4522 F	REAL			26	58			
4523 G	REAL			26	58			
4524 H	REAL			26	58			
4525 I	REAL			26	58			
4526 J	REAL			26	58			
4527 K	REAL			26	58			
4528 L	REAL			26	58			
4529 M	REAL			26	58			
4530 N	REAL			26	58			
4531 O	REAL			26	58			
4532 P	REAL			26	58			
4533 Q	REAL			26	58			
4534 R	REAL			26	58			
4535 S	REAL			26	58			
4536 T	REAL			26	58			
4537 U	REAL			26	58			
4538 V	REAL			26	58			
4539 W	REAL			26	58			
4540 X	REAL			26	58			
4541 Y	REAL			26	58			
4542 Z	REAL			26	58			
4543 A	REAL			26	58			
4544 B	REAL			26	58			
4545 C	REAL			26	58			
4546 D	REAL			26	58			
4547 E	REAL			26	58			
4548 F	REAL			26	58			
4549 G	REAL			26	58			
4550 H	REAL			26	58			
4551 I	REAL			26	58			
4552 J	REAL			26	58			
4553 K	REAL			26	58			
4554 L	REAL			26	58			
4555 M	REAL			26	58			
4556 N	REAL			26	58			
4557 O	REAL			26	58			
4558 P	REAL			26	58			
4559 Q	REAL			26	58			
4560 R	REAL			26	58			
4561 S	REAL			26	58			
4562 T	REAL			26	58			
4563 U	REAL			26	58			
4564 V	REAL			26	58			
4565 W	REAL			26	58			
4566 X	REAL			26	58			
4567 Y	REAL			26	58			
4568 Z	REAL			26	58			
4569 A	REAL			26	58			
4570 B	REAL			26	58			
4571 C	REAL			26	58			
4572 D	REAL			26	58			
4573 E	REAL			26	58			
4574 F	REAL			26	58			
4575 G	REAL			26	58			
4576 H	REAL			26	58			
4577 I	REAL			26	58			
4578 J	REAL			26	58			
4579 K	REAL			26	58			
4580 L	REAL			26	58			
4581 M	REAL			26	58			
4582 N	REAL			26	58			
4583 O	REAL			26	58			
4584 P	REAL			26	58			
4585 Q	REAL			26	58			
4586 R	REAL			26	58			
4587 S	REAL			26	58			
4588 T	REAL			26	58			
4589 U	REAL			26	58			
4590 V	REAL			26	58			
4591 W	REAL			26	58			
4592 X	REAL			26	58			
4593 Y	REAL			26	58			
4594 Z	REAL			26	58			
4595 A	REAL			26	58			
4596 B	REAL			26	58			
4597 C	REAL			26	58			
4598 D	REAL			26	58			
4599 E	REAL			26	58			
4600 F	REAL			26	58			
4601 G	REAL			26	58			
4602 H	REAL			26	58			
4603 I	REAL			26	58			
4604 J	REAL			26	58			
4605 K	REAL			26	58			
4606 L	REAL			26	58			
4607 M	REAL			26	58			
4608 N	REAL			26	58			
4609 O	REAL			26	58			
4610 P	REAL			26	58			
4611 Q	REAL			26	58			
4612 R	REAL			26	58			
4613 S	REAL			26	58			
4614 T	REAL			26	58			
4615 U	REAL			26	58			
4616 V	REAL			26	58			
4617 W	REAL			26	58			
4618 X	REAL			26	58			
4619 Y	REAL			26	58			
4620 Z	REAL			26	58			
4621 A	REAL			26	58			
4622 B	REAL			26	58			
4623 C	REAL			26	58			
4624 D	REAL			26	58			
4625 E	REAL			26	58			
4626 F	REAL			26	58			
4627 G	REAL			26	58			
4628 H	REAL			26	58			
4629 I	REAL			26	58			
4630 J	REAL			26	58			
4631 K	REAL			26	58			
4632 L	REAL			26	58			
4633 M	REAL			26	58			
4634 N	REAL			26	58			
4635 O	REAL			26	58			
4636 P	REAL			26	58			
4637 Q	REAL			26	58			
4638 R	REAL			26	58			
4639 S	REAL			26	58			
4640 T	REAL			26	58			
4641 U	REAL			26	58			
4642 V	REAL			26	58			
4643 W	REAL			26	58			
4644 X	REAL			26	58			
4645 Y	REAL			26	58			
4646 Z	REAL			26	58			
4647 A	REAL			26	58			
4648 B	REAL			26	58			
4649 C	REAL			26	58			
4650 D	REAL			26	58			
4651 E	REAL			26	58			
4652 F	REAL			26	58			
4653 G	REAL			26	58			
4654 H	REAL			26	58			
4655 I	REAL			26	58			
4656 J	REAL			26	58			
4657 K	REAL			26	58			
4658 L	REAL			26	58			
4659 M	REAL			26	58			
4660 N	REAL			26	58			
4661 O	REAL			26	58			
4662 P	REAL			26	58			
4663 Q	REAL			26	58			
4664 R	REAL			26	58			
4665 S	REAL			26	58			
4666 T	REAL			26	58			
4667 U	REAL			26	58			
4668 V	REAL			26	58			
4669 W	REAL			26	58			
4670 X	REAL			26	58			
4671 Y	REAL			26	58			
4672 Z	REAL			26	58			
4673 A	REAL			26	58			
4674 B	REAL			26	58			
4675 C	REAL			26	58			
4676 D	REAL			26	58			
4677 E	REAL			26	58			
4678 F	REAL			26	58			
4679 G	REAL			26	58			
4680 H								



# APPENDIX B

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FTN 4.5-434

74/74 OPT-1

PROGRAM EXPDIFP

STATEMENT LABELS	DEF LINE	REFERENCES
4121 10	12	04
4122 20	14	13
4123 30	23	18
4124 40	36	29
4125 50	44	25
4126 60	54	47
4127 70	62	24
4128 80	83	82
4129 90	85	84
COMMON BLOCKS	LENGTH	MEMBERS
A	5	DIAS NAME(LENGTH)
B	20000	0 R (11)
		3 RU (11)
		0 T (5000)
		15000 TERR (5000)
STATISTICS		
PROGRAM LENGTH	4148	248
BUFFER LENGTH	61028	2115
CH LABELED COMMON LENGTH	470458	20005

1 EPS (11)  
4 S (11)  
5000 E (5000)  
2 0 (11)  
10000 DELTA (5000)

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PTN 4.5+414

76/74 OPT-1

SUBROUTINE FCALC

```

1 SUBROUTINE FCALC(I,FOFTE,FSUBT,FSUDE,FSUBTT,FSUBTE)
  REAL JC,MU,NE
  COMMON/IR/EP5,0,MU,5
  COMMON/UT/TS0001,E(5000),DELTA(5000),TERR(5000)
  RT=RT(I)
  FOFTE=(JC(I)-QMU*NE(I)*E(I)*EXP(RT))/EPS
  FSUDE=(JC(I)-QMU*NE(I)*E(I)*EXP(RT))/EPS
  FSUBTT=(JC(I)-QMU*NE(I)*E(I)*EXP(RT))/EPS
  FSUBTE=(JC(I)-QMU*NE(I)*E(I)*EXP(RT))/EPS
  RETURN
END

```

## SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES
3 FCALC	1	11

VARIABLES	SM	TYPE	RELOCATION
23420 DELTA	REAL	ARRAY	B
23430 E	REAL	ARRAY	B
1 EPS	REAL	ARRAY	A
0 FOFTE	REAL	F.P.	
0 FSUDE	REAL	F.P.	
0 FSUBTT	REAL	F.P.	
0 FSUBTE	REAL	F.P.	
0 I	INTEGER	T.P.	

3 MU	REAL	A	REFS
2 0	REAL <td>A <td>REFS</td> </td>	A <td>REFS</td>	REFS
0 R	REAL <td>A <td>REFS</td> </td>	A <td>REFS</td>	REFS
113 RT	REAL <td>A <td>REFS</td> </td>	A <td>REFS</td>	REFS
4 S	REAL <td>A <td>REFS</td> </td>	A <td>REFS</td>	REFS
0 T	REAL <td>ARRAY</td> <td>B</td>	ARRAY	B
35230 TERR	REAL <td>ARRAY</td> <td>B</td>	ARRAY	B

EXTERNALS	EXP	JC	NE	TYPE	ANGS	REFERENCES
REAL	1	2	6	7	10	
REAL	1	2	6	7	9	
REAL	1	2	6	7	8	

COMMON BLOCKS	LENGTH	MEMBERS - DIAS NAME(LENGTH)
A	5	0 B (1)
B	20000	3 MU (1)
		0 T (5000)
		15000 TERR (5000)

STATISTICS	PROGRAM LENGTH	76
CM LABELED COMMON LENGTH	470450	20005

1 EPS	(1)	2 0	(1)
4 S <td>(1) <td>1000 DELTA <td>(5000)</td> </td></td>	(1) <td>1000 DELTA <td>(5000)</td> </td>	1000 DELTA <td>(5000)</td>	(5000)
5000 E <td>(5000)</td> <td></td> <td></td>	(5000)		



## SUBROUTINE GCALC

```

SUBROUTINE SCALC(I1,COFTE,CSUMT,CSUDE,CSUMTE)
  REAL C,MU,RE
  COMMON/7/TS000,I,E(1500),DELTA(1500),TERR(1500)
  I=407(I1)
  CSUMT=(JC(I1)-Q(MU)E(I1))/EPS
  CSUMT=(Q(MU)E(I1)+I)/EPS
  CSUDE=(Q(MU)E(I1))/EPS
  CSUMTE=(Q(MU)SI)/EPS
  RETURN
END

```

SYMBOLIC REFERENCE MAP (R-3)[illegible]

STATISTICS	
PROGRAM LENGTH	410
CM LABELED COMMON LENGTH	470458
	20005

```

1  SUBROUTINE DTWRITE(N,DEL,TSTART,THAX)
COMMON/87/(5000),E(5000),DELTA(5000),TERR(5000)
17-0
5  K=1
WRITE(6,10)
10  FORMAT(1M1)
WRITE(6,20)DEL,TSTART,THAX,M
20  FORMAT(1X,17DELTA TIME STEPS,1PE10.3,5X,15MSTARTING TIME,
11PE10.3,5X,20MAXIMUM TIME TO BE PLOTTED,1PE10.3,/,3X,
22MINCUMENT OF OUTPUT VALUES,15,/,/,/)
10  30  WRITE(6,30)
30  FORMAT(1X,4M TIME,14X,1ME,7X,1MTRUNCATION ERROR,8X,SHDELTA)
WRITE(6,40)
40  FORMAT(1X,4M-----,14X,1M-,7X,1M-----,8X,SH-----)
DO 110 I=1,M
115  WRITE(6,50)I(1),E(I),TERR(I),DELTA(I)
50  FORMAT(1X,4(1PE11.4,2X))
IF(I1T-EG,1) GO TO 60
IF(I1E-EG,50) GO TO 70
IF(I1F-EG,60) GO TO 70
60  K=K+1
GO TO 110
70  CONTINUE
WRITE(6,80)
80  FORMAT(1M1)
WRITE(6,90)
90  FORMAT(1X,4M TIME,14X,1ME,7X,1MTRUNCATION ERROR,8X,SHDELTA)
100  WRITE(6,100)
100  FORMAT(1X,4M-----,14X,1M-,7X,1M-----,8X,SH-----)
17-1
K=1
110  CONTINUE
RETURN
END

```

## SYMBOLIC REFERENCE MAP (R-3)

[illegible]



# APPENDIX B

SUMROUTINE DTURIT			74/74	OPT-1	FTN 4.5-414			06/04/76	13.30.36	PAGE	2
FILE NAMES	MODE										
TAPES	PRT	WRITES	5	7	11	13	16	24	26	28	
STATEMENT LABELS		DEF LINE	REFERENCES								
70 10	PRT	6	5								
101 20	PRT	8	7								
124 30	PRT	12	11								
135 40	PRT	14	13								
192 50	PRT	17	16								
64 60	PRT	20	18								
50 70	PRT	23	19								
160 80	PRT	25	24								
165 90	PRT	27	26								
276 100	PRT	29	28								
60 110	PRT	32	31								
LOOPS LABEL		FROM-TO	LENGTH	PROPERTIES		EXT REFS					
30 110	0 1	15 32	338								
COMMON BLOCKS		LENGTH	MEMBERS - DIAS NAME(LENGTH)		5000 E (5000)		10000 DELTA (5000)				
0	20000	0 T (5000)									
		15000 TERA (5000)									
STATISTICS		PROGRAM LENGTH	2218	145							
COMMON LENGTH		476408	20000								
CN LABELED COMMON LENGTH											

SYMBOLIC REFERENCE MAP (R=3)

STATISTICS		
PROGRAM	LENGTH	
CN	LABELLED	COMMON
	408	32
	470408	20000



```

3      REAL FUNCTION NE(II)
      REAL NEO
      COMMON/PA/REPS,Q,MU,S
      COMMON/PT/TSOONO,I*(5000),DELTA(5000),TERR(5000)
      NEO=1.133E+11
      IF (II).GE.O.) GO TO 10
      C NE MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
      NE=NEO*1.E+6
      RETURN
      C NE MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
      10 NE=(NEO+S*(II))*1.E+6
      RETURN
      END

```

STATISTICS	
PROGRAM LENGTH	240
CN LABELED COMMON LENGTH	470450
	20005

007-1

10 JC-1.34E+3

## SYMBOLIC REFERENCE MAP (R-3)

COMMON BLOCKS	LENGTH	MENDERS - DIAS	NAME(LENGTH)
A	5	0 R	(11)
		3 MU	(11)
B	20000	0 T	(15000)
		15000 TEAR	(15000)



# APPENDIX B

PAGE 1

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FTN 4.6420

74/74 OPT=1

SUBROUTINE PRTPLOT

1 C SUBROUTINE PRTPLOT (HORZ,VERT,NPTS,HEAD,HLAB,VLAB,HREF,VREF,J)  
C THIS FORTRAN SUBROUTINE PRODUCES A FULL PAGE X-Y PRINTER PLOT.

5 C HORZ - REAL ARRAY TO BE PLOTTED ALONG HORIZONTAL AXIS.  
C VERT - REAL ARRAY TO BE PLOTTED ALONG VERTICAL AXIS.

10 C NPTS - NUMBER OF VALUES IN HORZ,VERT (NTE 101)  
C HEAD - PLOT HEADING (MUST BE 5 WORDS)

15 C HLAB - LABEL FOR HORIZONTAL AXIS (MUST BE 3 WORDS)  
C VLAB - LABEL FOR VERTICAL AXIS (MUST BE 3 WORDS)

20 C HREF - REFERENCE VALUE FOR HORIZONTAL AXIS.  
C VREF - REFERENCE VALUE FOR VERTICAL AXIS.

25 C J - THIS DETERMINES THE SIZE OF THE ARRAYS HORZ AND VERT--NTE 100  
C

30 C DIMENSION HORZ(J),VERT(J),HEAD(5),HLAB(3),VLAB(3),LINE(101),  
C IVER(101),JHOR(101),JVERT(101),VERTIC(101),VAXIS(30),DOWNT(21)  
C INTEGER BLANK,STAR,DOT,EYE

35 C DATA BLANK/IN /,STAR/IN/,DOT/IN/,MINUS/IN/,EYE/IN/

40 C CALL DATE(10AT)  
C CALL TIME(10T)

45 C HEAD(5)=DAT  
C HEAD(5)=TIM

50 C MD = 1  
C NUN = 1

55 C N = NPTS  
C N = MIN(101,N)

60 C DO 10 I = 1,N  
C HORZ(I) = HORZ(I)

65 C VERTIC(I) = VERT(I)  
C 10 CONTINUE

70 C DECODE (30,1000,VLAB(1)) (VAXIS(1),1-1,30)  
C 1000 FORMAT(30A1)  
C 20 NA = N - 1

75 C DO 30 I = 1,NA  
C IF (VERTIC(I).GE.VERTIC(I+1)) GO TO 30

80 C HOLD = VERTIC(I)  
C VERTIC(I) = VERTIC(I+1)

85 C VERTIC(I+1) = HOLD  
C SAVE = HORZ(I)

90 C HORZ(I) = HORZ(I+1)  
C HORZ(I+1) = SAVE

95 C 30 CONTINUE

100 C DO 40 I = 1,NA  
C IF (VERTIC(I).LT.VERTIC(I+1)) GO TO 20

105 C 40 CONTINUE

110 C VMAX = VERTIC(1)  
C VMIN = VERTIC(N)

115 C HMAX = HORZ(1)  
C HMIN = HORZ(N)

120 C DO 50 I = 2,N

```

55      MZ = MOD12(1)
      HMAX = AMAX(HMAX,MZ)
      HMIN = AMIN(HMIN,MZ)
      50 CONTINUE
      DO 60 I = 1,N
      JVER = 50.0*(VERTIC(1)-VMIN)/(VMAX-VMIN) + 1.5
      IVER(1) = 52 - JVER
      60 JHOR(1) = 100.0*(HOR12(1)-HMIN)/(HMAX-HMIN) + 1.5
      KREF = 100.0*(HREF-HMIN)/(HMAX-HMIN) + 1.5
      IF (KREF-1.1) KREF = 150
      IF (KREF-1.1) KREF = 150
      KREF = 50.0*(HREF-VMIN)/(VMAX-VMIN) + 1.5
      KREF = 52 - KREF
      IF (KREF-1.1) KREF = 1
      IF (KREF-1.1) KREF = 1
      UP = (VMAX-VMIN)/50.
      PRINT 200, HEAD
      200 FORMAT(1H,35H,5A10//)
      DO 200 N = 1,51
      LINE(1) = EYE
      LINE(1) = EYE
      DO 70 I = 2,100
      70 LINE(1) = BLANK
      IF (K-EJ.1) GO TO 90
      IF (K-EJ.51) GO TO 90
      IF (K-NE-KREF) GO TO 120
      DO 80 I = 2,100
      80 LINE(1) = DOT
      GO TO 120
      90 DO 100 I = 2,100
      100 LINE(1) = MINUS
      DO 110 I = 6,100,5
      110 LINE(1) = EYE
      GO TO 130
      120 IF (KREF-EQ.150) GO TO 130
      IF (KREF-EQ.1) GO TO 130
      LINE(KREF) = DOT
      130 IF (K-EQ.IVER(NUM)) GO TO 140
      IF (K-LT.IVER(NUM)) GO TO 160
      NUM = NUM + 1
      GO TO 130
      140 IF (JHOR(NUM)-GT.101) GO TO 150
      IF (JHOR(NUM)-LT.1) GO TO 150
      JH = JHOR(NUM)
      LINE(JH) = STAR
      150 NUMBER = NUM + 1
      IF (IVER(NUM)-NE.IVER(NUMBER)) GO TO 160
      NUM = NUMBER
      GO TO 140
      160 T = N - 1
      OPT = VMAX - T*UP
      IF (K-LT.11) GO TO 170
      IF (K-GT.41) GO TO 170

```



# APPENDIX B

PAGE 3

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PTM 4.8+420

SUBROUTINE PRTPY 74/74 OPT=1

```

110      TARI5 = TARI5(MO)
        MC = MC + 1
        PRINT 3000, TARI5, UPT, LINE
        3000 FORMAT(4X, A1, 4X, 1P E9.2, 2X, 10I A1)
        GO TO 200
115      170 PRINT 4000, UPT, LINE
        4000 FORMAT(9X, 1P E9.2, 2X, 10I A1)
        200 CONTINUE
        OLUN = (MMAX-MMIN)/20.
        T = MMIN
        DO 210 I = 1, 21
          DOWN(I) = T
          T = T + DOWN
210      CONTINUE
        5000 PRINT 5000, (DOWN(I), I=1, 21, 2)
        5000 FORMAT(15X, 1P I E10.2)
        6000 PRINT 6000, (DOWN(I), I=2, 20, 2)
        6000 FORMAT(20X, 1P I E10.2)
        PRINT 7000, M, LAB
        7000 FORMAT(150X, 3A10)
        RETURN
        END

```

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